

WHEEL

Defect Prevention Research Consortium

Findings of the Wheel Defect Prevention Research Consortium

Scott Cummings
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◆ The basics

- Who – are we?
- What – is the goal?
- Why – are we motivated?
- How – do we approach the problem?

◆ Findings

- Shelling vs. Spalling – Inspections of wheelsets
- Spalling
- Shelling
 - ◆ Rolling Contact Fatigue
 - ◆ Thermal Mechanical Shelling

◆ Recommendations

◆ Ongoing work

Who?

- ◆ **WDPRC = Wheel Defect Prevention Research Consortium**
- ◆ **Government, Railroads, Private Car Owners, Suppliers**
 - American Electric Power
 - Amsted Rail (Griffin Wheel)
 - BNSF
 - CIT
 - Canadian Pacific Railway
 - CSX Transportation
 - Federal Railroad Administration
 - GATX
 - GE Rail
 - Holland Company
 - Norfolk Southern
 - New York Air Brake
 - Progress Rail
 - Standard Car Truck Co. (Anchor Brake Shoe, Zeftek)
 - Standard Steel
 - Sumitomo
 - TTCI
 - TTX
 - Union Tank Car
 - Union Pacific Railroad
 - Wabtec (Cardwell Westinghouse, Railroad Friction Products Corp.)

What?

- ◆ Find root causes of wheel tread damage and identify remedies
- ◆ Two major categories of wheel tread damage:

- Slid flats and spalling: wheel sliding on rail creates enough heat to produce a metallurgical transformation and eventually produce a spall

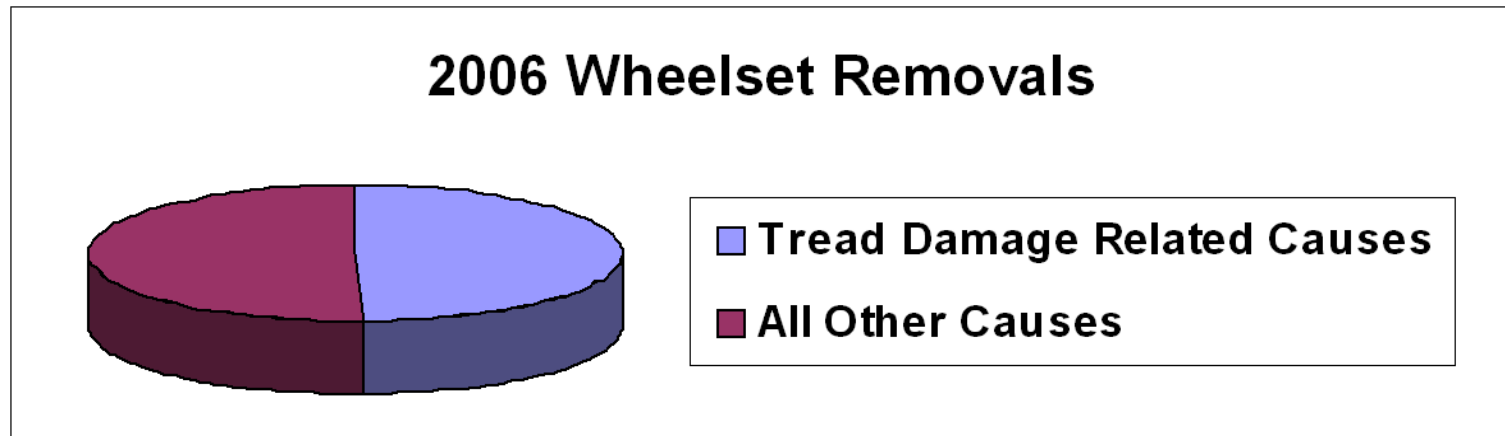
- Fatigue and shelling: repeated cycling of stresses causes cracks to form and eventually produce a shell





Why?

- ◆ Tread damage → Impact loads → Damage to track and car
- ◆ Almost half of the 700,000 wheelsets changed out in 2006 were due to tread damage related causes (WMC 61, 65, 67, 75, and 78)
- ◆ Approximate cost in 2006: \$350 million



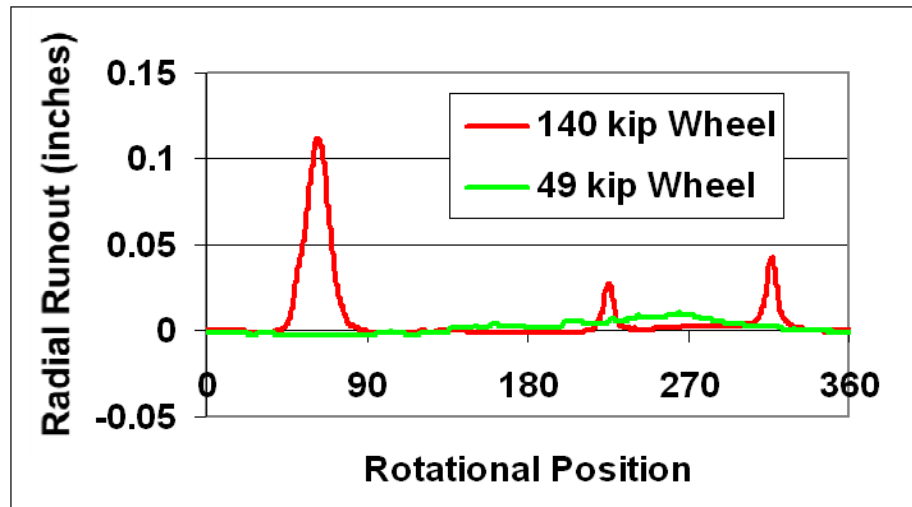
How?

- ◆ **WDPRC utilizes diverse data sources to determine root cause**
 - Existing literature
 - Inspections
 - ◆ Damaged and undamaged wheelsets
 - ◆ Good and bad actor cars
 - Controlled condition testing
 - ◆ Air brake valves
 - ◆ Brake shoe force
 - ◆ Drag brake thermal testing
 - Analysis of data from wayside detectors
 - ◆ WILD (wheel impact load detector)
 - ◆ Wheel temperature
 - Computer simulation
 - ◆ Wheel sliding
 - ◆ Wheel fatigue



Findings: Shelling Vs Spalling

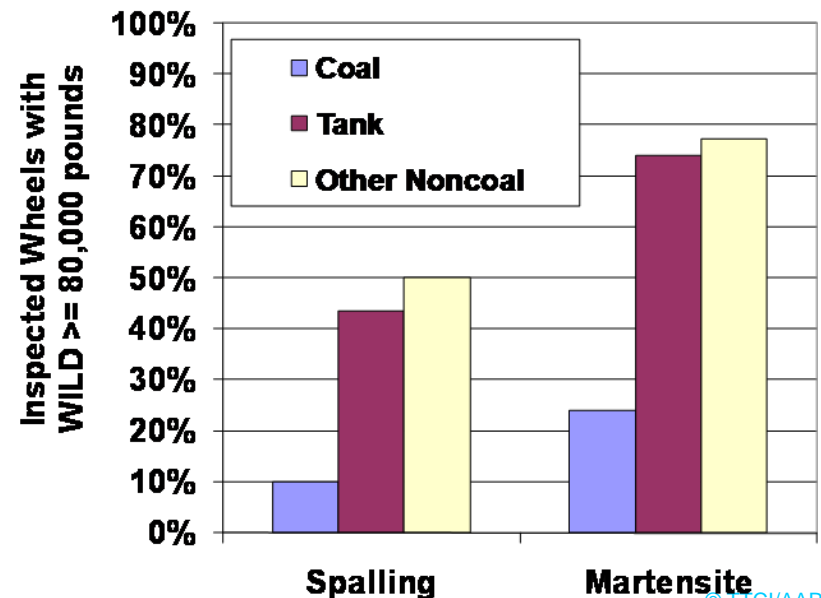
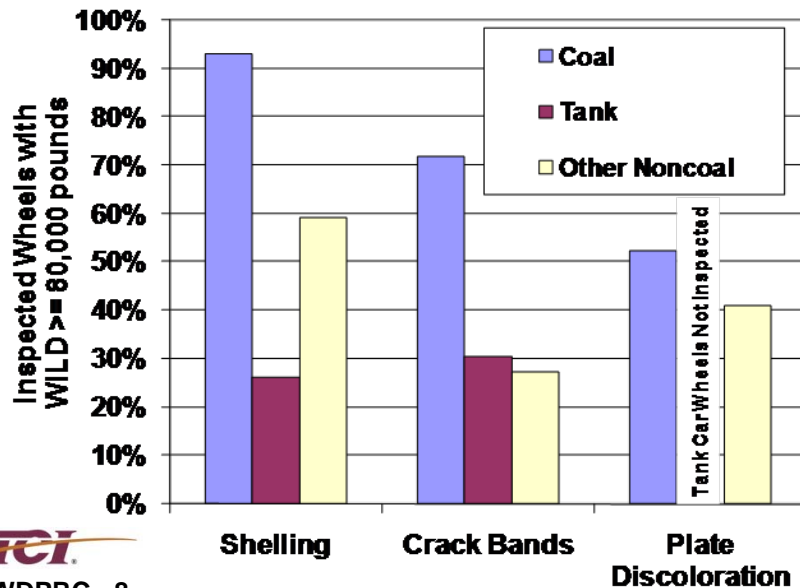
- ◆ 163 wheelsets inspected at three shops (WMC 11,61,64,65)
- ◆ Etchant applied, radial runout recorded, expert observation
- ◆ Type of damage tied to car type and service
 - Coal cars = shelling
 - Noncoal cars = mix of spalling and shelling (primarily spalling)
 - Intermodal = thermal mechanical shelling according to car owner



Findings: Shelling Vs. Spalling

- ◆ Based on CRB data, overall wheel tread damage problem is split about evenly between shells and spalls
- ◆ Noncondemnable defects found on many wheels removed for wear causes: tread damage more prevalent than repair records indicate

Car Type	Sample Size	Shelling Found	Spalling Found
Coal Hoppers and Gondolas	71	93%	10%
Tank Cars	23	26%	44%
Covered Hoppers	12	42%	58%
Mill Gondolas	7	71%	43%



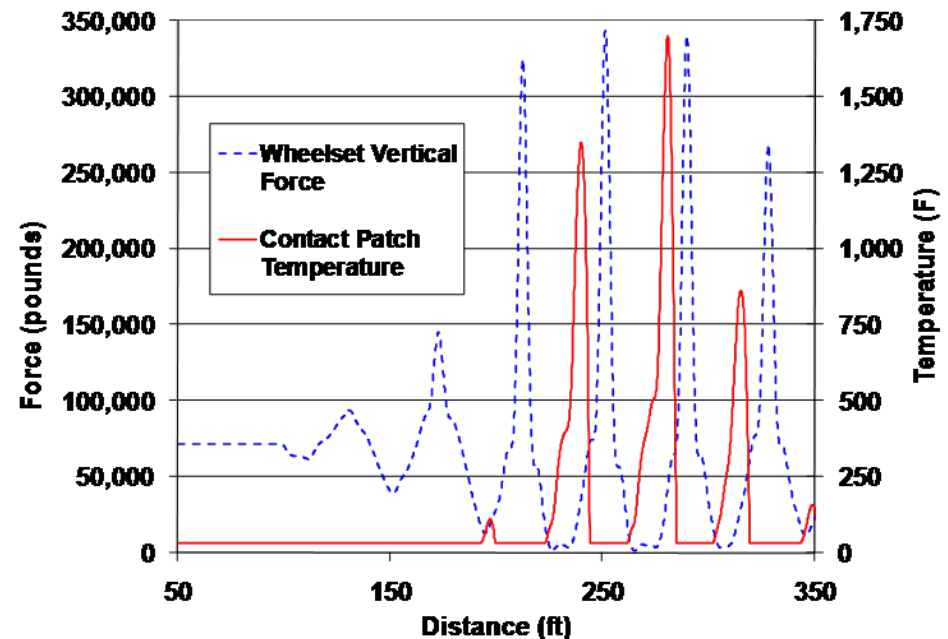
◆ Literature Review

- Wheel slide tests show that the potential exists to create martensite on sliding wheels with almost any realistic combination of axle load, wheel slide duration, train speed, and wheel/rail adhesion level¹
- Maximum wheel slide contact patch temperatures are probably achieved within the first second of a constant velocity wheel slide²
- Multiple authors note presence of spalling on one wheel with none on the mate
 - ◆ Different adhesion levels on each rail, such that one wheel reaches austenitizing temperature while the other does not²
 - ◆ Very short duration slide where one wheel stays in synchronous contact with the rail³
 - ◆ Different wear rates between wheels on same wheelset⁴

- 1) Jergeus, J., Odenmarck, C., Lunden, R., Sotkovski, P., Karlsson, B., and Gullers, P., "The Silinge Wheel Flat Experiments," Report F202, Department of Solid Mechanics, Chalmers University of Technology, Gothenburg, Sweden, 1997.
- 2) Sawley, K.J., and J.A. Rosser, "Tread Damage in Disc-Braked Wheels", 9th International Wheelset Congress, Montreal, Canada, Sept 1988.
- 3) Bartley, G.W., "A Practical View of Wheel Tread Shelling", 9th International Wheelset Congress, Montreal, Canada, Sept 1988.
- 4) Magel, E., and J. Kalousek, "Martensite and Contact Fatigue Initiated Wheel Defects", 12th International Wheelset Congress, Qingdao, China, Sept 1998.

◆ NUCARS^{®1} simulations

- Traversing rough track designed to excite suspension bounce resonance
 - ◆ Brake retarding forces applied and wheelset rotational speeds calculated, contact patch temperatures estimated
 - ◆ Traversing rough track with brakes applied is probably not a major source of spalling for loaded cars
- Empty cars (and especially those with malfunctioning E/L device) can slide wheels under heavy braking in low wheel/rail friction conditions regardless of track geometry. This may be a minor source of spalling



- ◆ **Movement of cars with handbrakes applied is a major source of wheel spalling**
 - Numerous analyses have been conducted in the past that show cars with truck mounted brakes have more tread damage to the wheels on the “B” end
 - WDPRC found 95% / 5% split in this case for a group of 294 tank cars
- ◆ **In 2007, WDPRC updated a training video about the importance of releasing handbrakes**
 - “Please Release Me...Let Me Roll”
 - Target audience is operating personnel
 - Free, downloadable version at www.aar.com/wdprc
 - Free DVD versions available to training organizations by emailing this presenter with a request and your mailing address
 - ◆ Scott_Cummings@ttci.aar.com

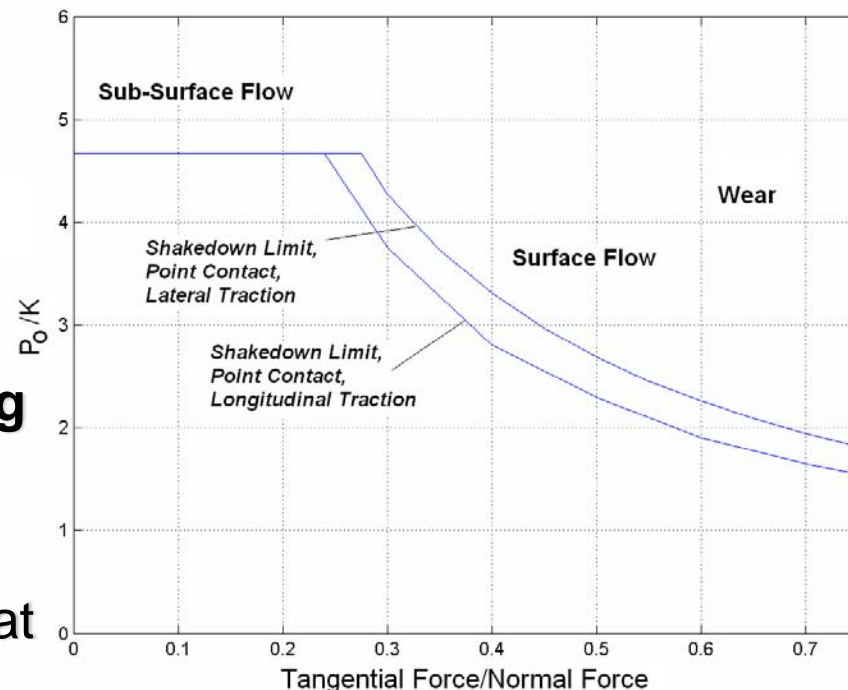
◆ RCF = Rolling Contact Fatigue

- Many cycles of high stress (tangential forces)
- Shakedown predicts RCF by relating
 - ◆ Ratio of tangential force to normal force (T/N)
 - ◆ Ratio of contact stress to shear yield strength (P_0/K)

◆ TMS = Thermal Mechanical Shelling

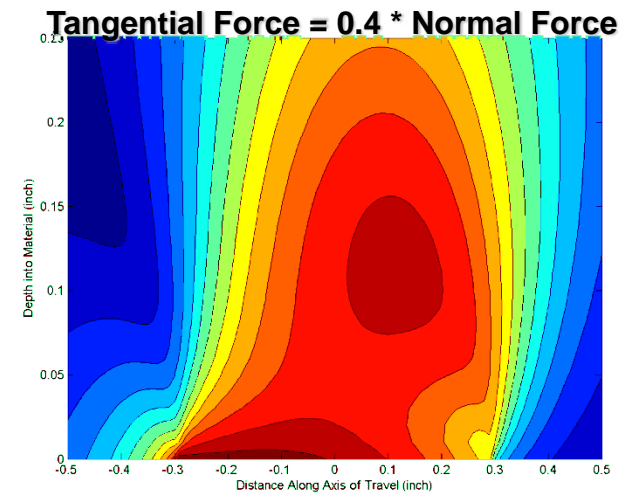
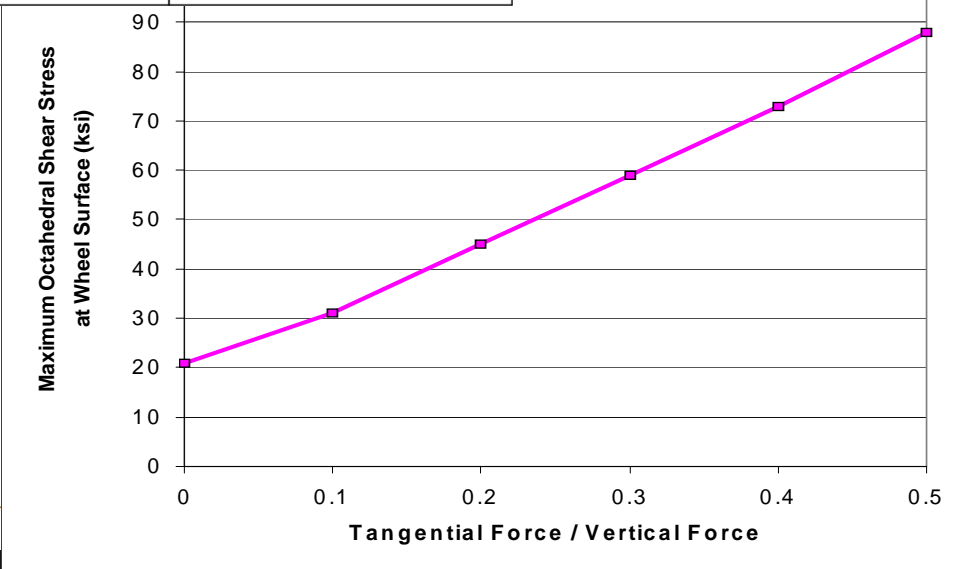
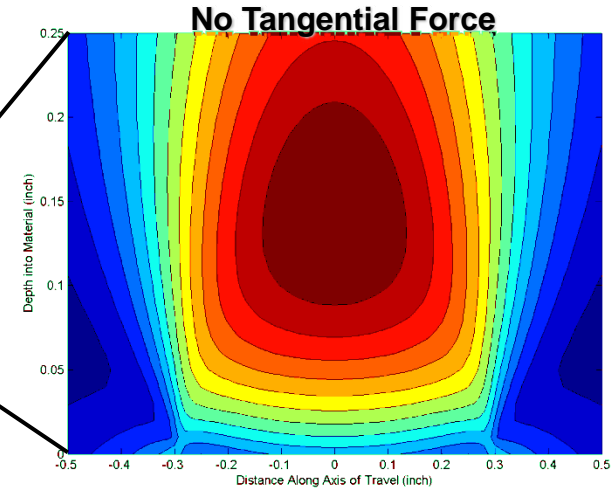
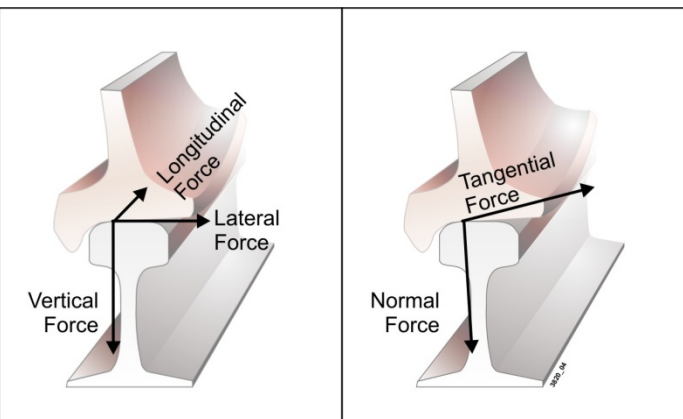
- Subset of shelling – requires hot wheels
- Resistance to fatigue is reduced at high temperatures
 - ◆ Steel properties degrade
 - ◆ Beneficial compressive residual hoop stresses are relieved

- Loaded car $P_0/K \sim 3$, therefore RCF @ T/N ~ 0.375
- T/N limited by wheel/rail COF
- Typical COF values 0.35 to 0.55



Background: Shelling - RCF

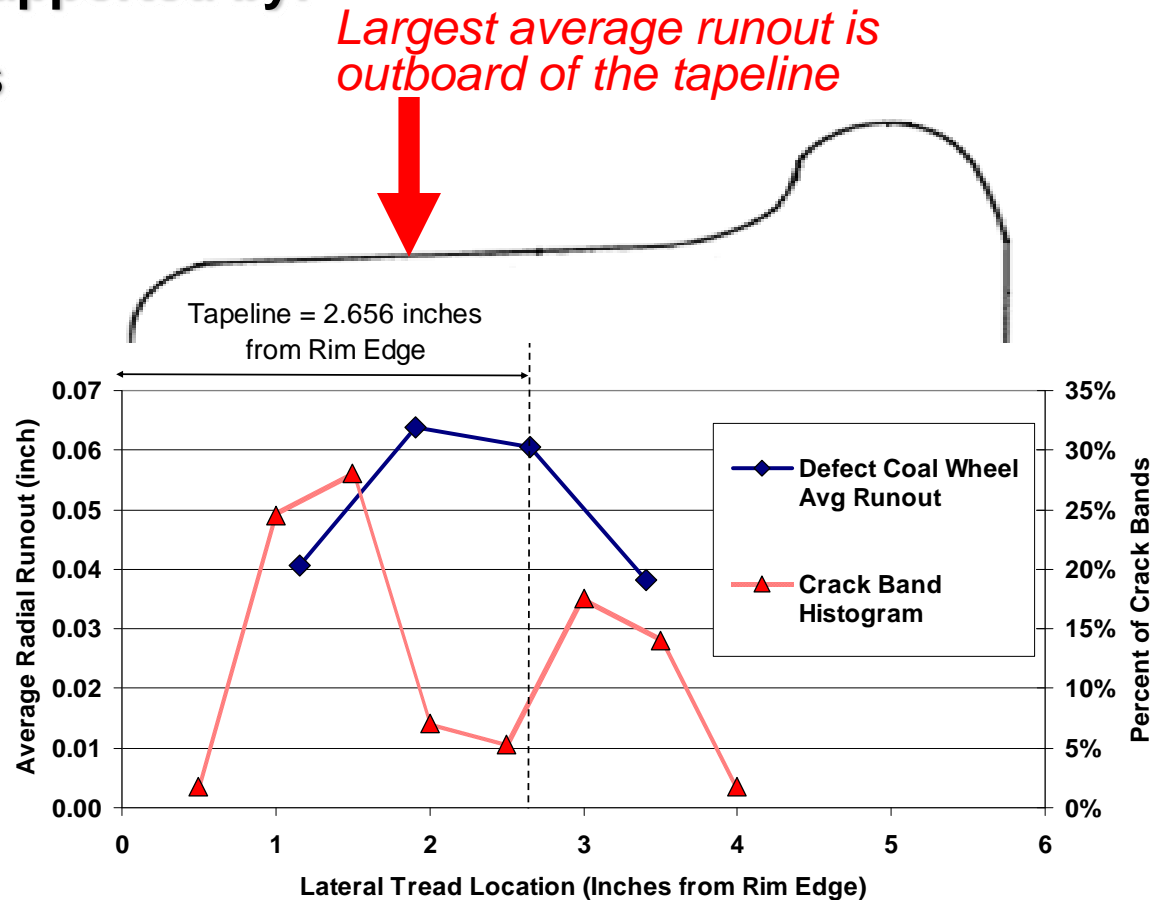
- ◆ Wheel/rail tangential forces are important to the stress near the tread surface where cracks initiate and propagate
 - Tangential forces move the stress closer to the tread surface



Findings: Shelling (RCF)

◆ Most RCF damage occurs on the low rail wheel of the wheelset in the lead position of the truck during curve negotiation of a loaded car. Finding supported by:

- Wheelset inspections
- Revenue service Instrumented Wheelset data
- NUCARS modeling
- WILD data analysis



Shelling Progression Photos

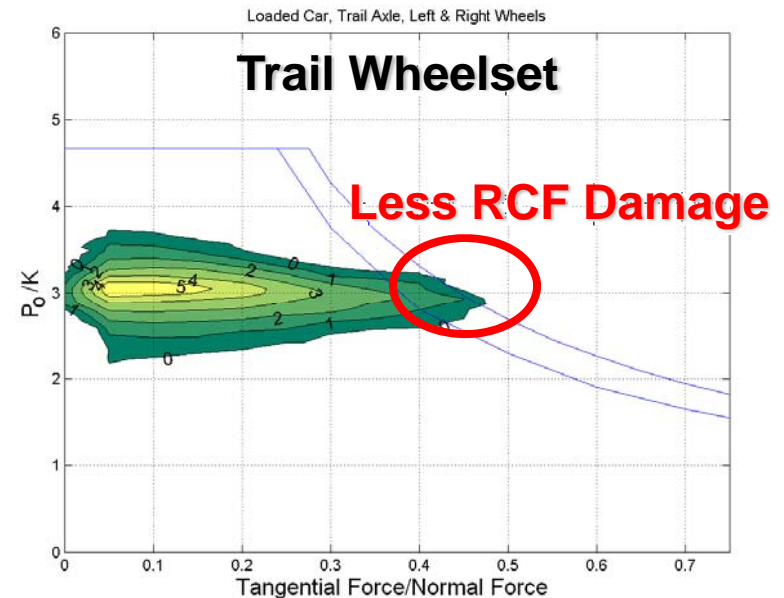
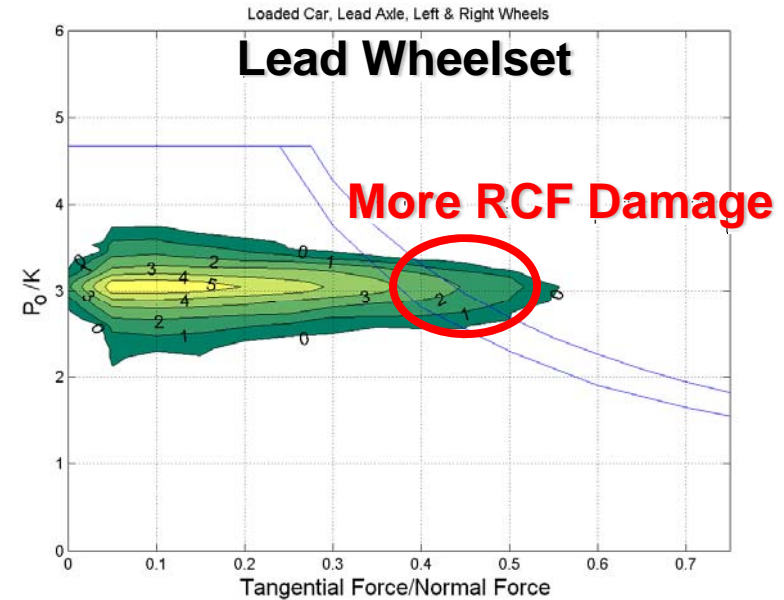
◆ Photos show wheel shells developing as follows:

1. Crack band appears outboard of tapeline
2. Cracks join to form shells
3. Shells grow inboard toward tapeline where contact with rail occurs on more regular basis



More Findings: Shelling (RCF)

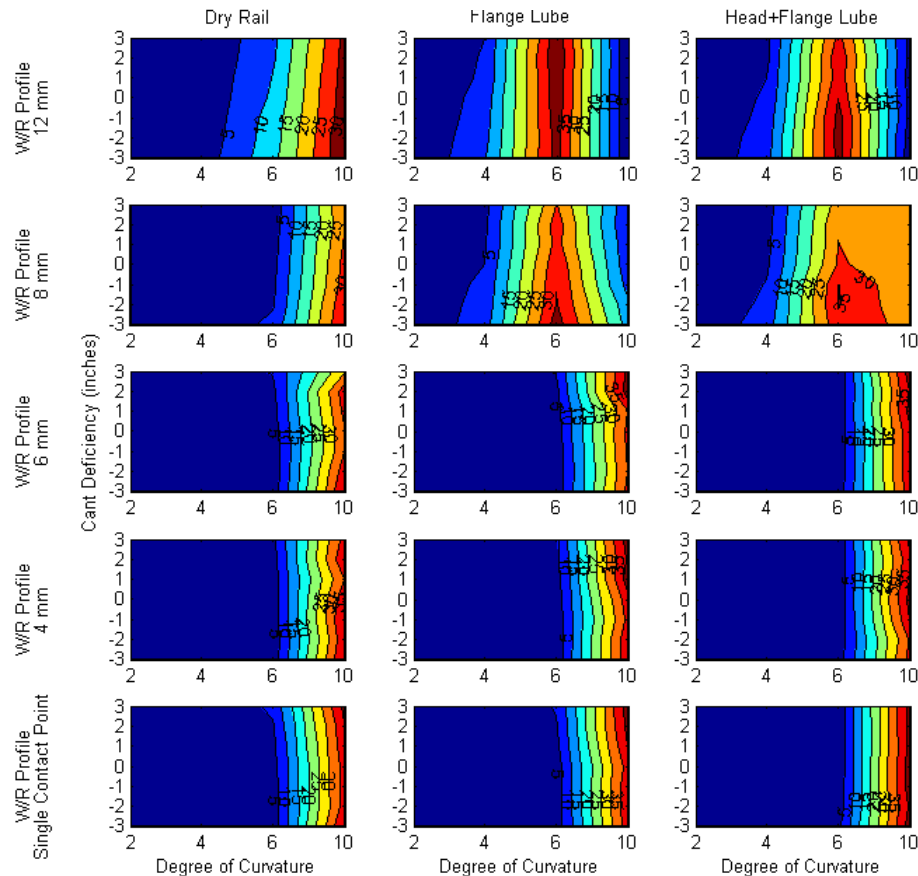
- ◆ Potential to reduce RCF with minor changes to track & operating conditions
- Data analyzed from instrumented wheelsets installed in a loaded coal car: 1,500 miles in revenue service
- Total distance traveled with predicted RCF damage: < 1 mile
- Most curves of 4 degrees or tighter caused some predicted RCF
- 4 specific locations accounted for half of *predicted* RCF damage
- Train typically operated below curve balance speed when RCF was predicted



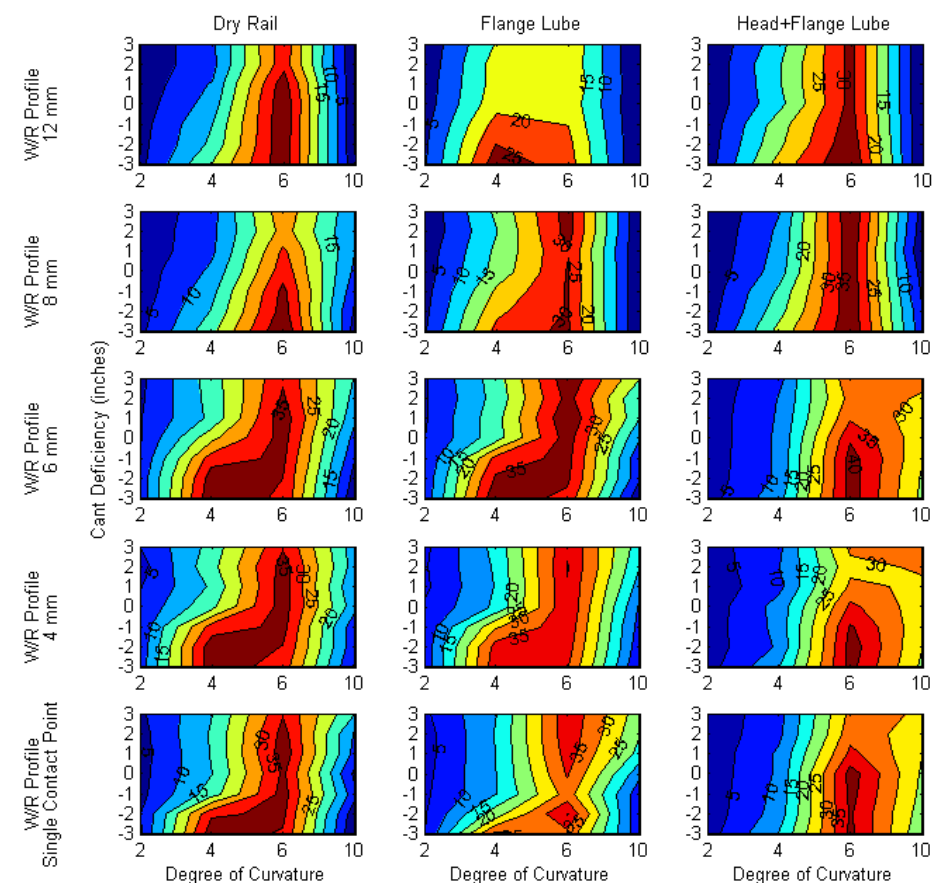
More Findings: Shelling (RCF)

- ◆ Potential to reduce RCF with improved trucks
 - NUCARS modeling of many condition combinations shows truck type to be important factor (red = RCF, blue = no RCF)

M-976 Truck



Standard Truck



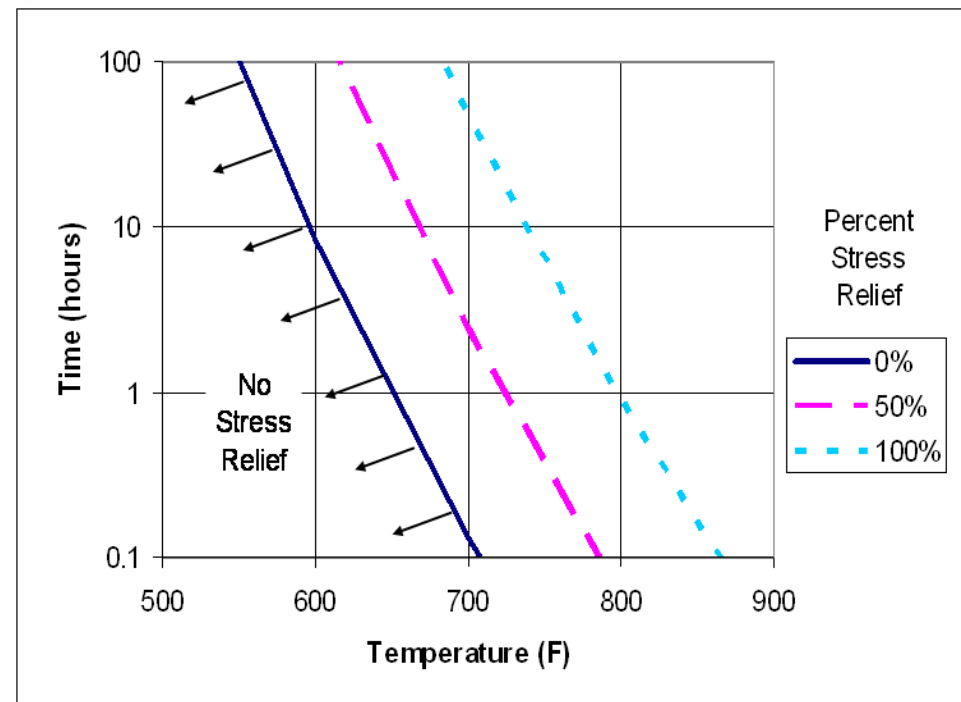
Findings: Shelling (TMS)

◆ Maximum acceptable operating tread temperature to avoid TMS is approximately 600°F

- Applying Larson-Miller equation to existing data allows time / temperature / % stress relief relationship
- Sines fatigue calculation shows that wheels are far more prone to shelling in the absence of compressive residual stress
- Short duration exposure allows higher temperatures

- Wheels with properly functioning brake systems do not typically reach 600°F

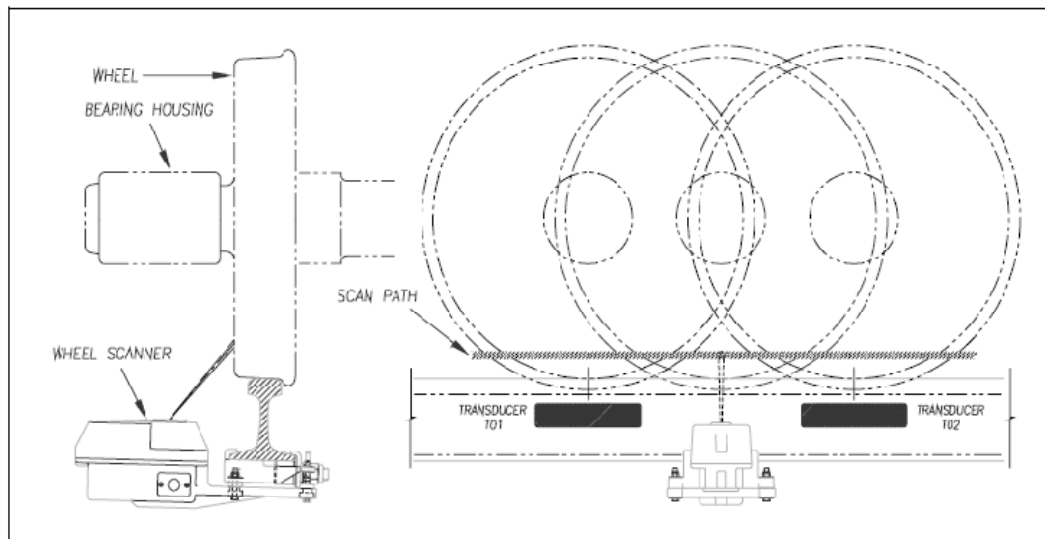
◆ Ex: 50 Hp for 30 minutes would produce 600°F¹



1) Stone, D.H., D.G. Blaine, and G.F. Carpenter. 1994. "Effect of High Horsepower Grade Braking on AAR High Friction Composition Shoes." *Proceedings of 86th Annual Convention and Technical Conference of the Air Brake Association*. Chicago, IL. pp. 113-135.

More Findings: Shelling (TMS)

- ◆ **Wheel temperature variations lead to hot wheels**
 - Data from a single wheel temperature detector installed near bottom of hill – 1,575 trains analyzed, over 600,000 wheelsets
 - Temperature variations found between trains
 - ◆ 15 trains accounted for more than 20% of the descending cars with hot wheels
 - Train handling can affect wheel temperature → shelling



Southern Technologies Corporation.
July 2004. "SmartScanS User's
Guide for Union Pacific," EUD-
2004194-PV, pp 137.

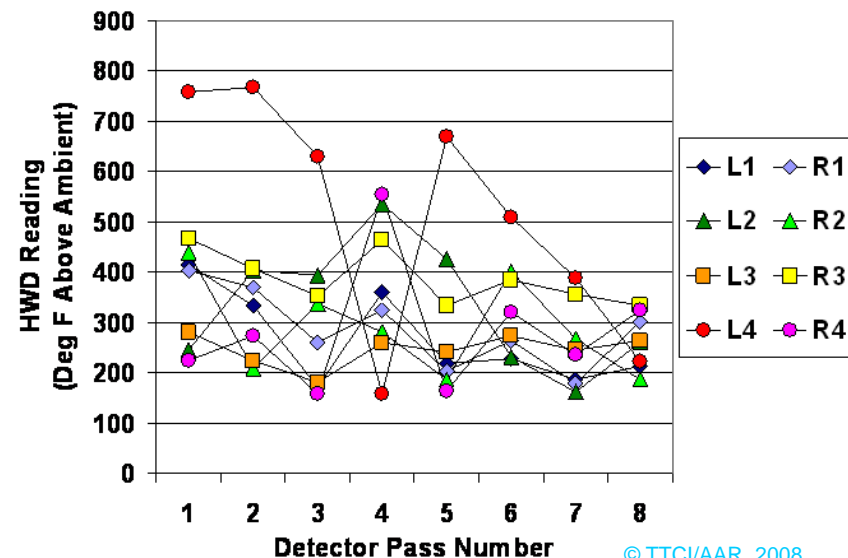
More Findings: Shelling (TMS)

- ◆ **Wheel temperature variations lead to hot wheels**
 - Data from a single wheel temperature detector installed near bottom of hill – 1,575 trains analyzed, over 600,000 wheelsets
 - Temperature variations found within cars and between cars
 - ◆ 76% of the descending cars with a wheel temperature greater than 500°F had only a single wheel above this level
 - ◆ While the wheels in these cars are generally at higher temperatures than the wheels of other cars in the train, there were large temperature differences between individual wheel locations
 - Repeated hot wheel behavior was found on
 - ◆ 37% of the descending cars with hot wheels
 - ◆ 20% of individual hot wheel locations



More Findings: Shelling (TMS)

- ◆ **The cause of hot wheel behavior within cars and between cars is difficult to identify**
 - Inspection shortly after passing temperature detector
 - ◆ 1 car found with handbrake applied, all wheels hot
 - ◆ No cause found for 14 other cars inspected
 - Detailed inspection/teardown/brake test
 - ◆ Good and bad actor cars selected based on multiple wheel temperature readings
 - ◆ Found one bad actor car with valve leaking air into brake cylinder
 - ◆ The selection of bad and good actor cars based on wheel temperatures correlated well with wheelset replacements
 - Bad actors had twice as many replacements



◆ Abridged list of WDPRC recommendations

- Increase adherence to handbrake release policies to reduce wheel spalling
 - ◆ Utilize “Please Release Me...Let Me Roll” in training programs
- Identify problem RCF curves and investigate
 - ◆ Rail profiles
 - ◆ Superelevation
 - ◆ Rail COF
- Reduce wheel/rail tangential forces during curve negotiation
 - ◆ Use trucks with high warp resistance and low axle steering resistance
- Minimize use of train brake by maximizing use of dynamic brake, especially in regions with heavy grades to obtain the minimum average wheel temperature per train

◆ Focus on implementing recommendations

- Proposed changes to single car test (AAR S-486) with evidence to support
- Distribute and promote “Please Release Me...Let Me Roll”
- Determine current state of industry with respect to dynamic brake training and usage
 - ◆ Possibly assist with industry standard training material
- Identify specific problem RCF curves
 - ◆ Determine why worse than other curves (profile, COF, geometry)?
 - ◆ Recommend specific course of action to correct
- Determine economics related to truck maintenance
 - ◆ Wheel savings could pay for improved truck maintenance
 - ◆ Recommend optimal ton-mileage for reconditioning
- Additional investigation into sources of wheel temperature variations within cars and between cars